### SUPPORTING INFORMATION

# Lithium Diisopropylamide: Nonequilibrium Kinetics and Lessons Learned About Rate Limitation

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# **I. Simulation Protocols**

# Generic Scheme.

Assuming the generic scheme

A 
$$\underbrace{k_1}_{k_{-1}}$$
 B  $\underbrace{k_2[C]}_{product}$  product

an expression for [B] at a steady state follows.

$$[B] = \frac{k_1[A]}{k_{-1} + k_2[C]}$$

From this expression one readily obtains the rate law for consumption of C.

$$-\frac{d[C]}{dt} = \frac{k_1 k_2 [A][C]}{k_{-1} + k_2 [C]}$$

# **II. Simulations**

All figures were generated in Igor Pro® using simulated data from Wolfram Mathematica®. Following each figure is a chemical scheme and demarcated Mathematica code that can be copied and directly executed to recreate the plots. The figure numbers correspond to those in the manuscript.



**Figure S1**. (Figure 2 in manuscript) Saturation kinetics. A and B correspond to regions of substrate-concentration-dependent and substrate-concentration-independent regions.

A 
$$\underbrace{\frac{k_1}{k_{-1}}}_{k_{-1}}$$
 B  $\underbrace{\frac{k_2[C]}{k_2[C]}}_{product}$ 

$$\frac{d[A]}{dt} = -k_1[A] + k_{-1}[B]$$

$$\frac{d[B]}{dt} = k_1[A] - k_{-1}[B] - k_2[B][C]$$

$$\frac{d[C]}{dt} = -k_2[B][C]$$

 $sol[k1\_, kn1\_, k2\_, a0\_, c0\_] := NDSolve[\{a'[t] == -k1*a[t] + kn1*b[t], b'[t] == k1*a[t] - kn1*b[t] - k2*b[t]*c[t], c'[t] == -k2*b[t]*c[t], a[0] == (a0 kn1)/(k1 + kn1), b[0] == (a0 k1)/(k1 + kn1), c[0] == c0\}, \{a, b, c\}, \{t, 0, 1000\}]$   $Manipulate[\{Plot[-c'[10] /. sol[k1, kn1, k2, a0, c0], \{c0, 0, 0.1\}, PlotRange -> \{0, 0.0001\}]\}, \{\{k1, 0.001, "k1"\}, 0, 10\}, \{\{kn1, 1, "kn1"\}, 0, 10\}, \{\{k2, 1000, "k2"\}, 0, 10\}, \{\{a0, 0.1, "a0"\}, 0, 10\}, \{\{c0, 0.01, "c0"\}, 0, 0.1\}]$ 

Export["table.xls", Table[-c'[10] /. sol[0.001, 1, 100, 0.1, x], {x, 0, 0.1, 0.001}]]



**Figure S2**. (Figure 4 in manuscript) Decays of substrate ArH according to eqs 5 and 6 assuming rate-limiting proton transfer  $(k_2[ArH]/k_{-1} = 0.1; \text{ curve A})$  and rate-limiting deaggregation  $(k_2[ArH]/k_{-1} = 10; \text{ curve B})$ .

$$A \xrightarrow{k_1} B \xrightarrow{k_2[C]} product$$

$$\frac{d[A]}{dt} = -k_1[A] + k_{-1}[B]$$

$$\frac{d[B]}{dt} = k_1[A] - k_{-1}[B] - k_2[B][C]$$

$$\frac{d[C]}{dt} = -k_2[B][C]$$

 $\begin{array}{l} \text{sol}[k1\_, kn1\_, k2\_, a0\_, c0\_] \coloneqq & \text{NDSolve}[\{a'[t] == -k1*a[t] + kn1*b[t], b'[t] == k1*a[t] - kn1*b[t] - k2*b[t]*c[t], c'[t] == -k2*b[t]*c[t], a[0] == (a0 \ kn1)/(k1 + kn1), b[0] == (a0 \ k1)/(k1 + kn1), c[0] == c0\}, \{a, b, c\}, \{t, 0, 10000\} \end{bmatrix}$ 

Export["table.xls", {Table[ Evaluate[c[t] /. sol[0.0001, 1, 10, 0.1, 0.01]], {t, 0, 50000, 10}], Table[ Evaluate[c[t] /. sol[0.0001, 1, 1000, 0.1, 0.01]], {t, 0, 5000, 1}]]}



**Figure S3**. (Figure 5 in manuscript) Zeroth-order decays at various initial starting concentrations of ArH showing parallel decays and the onset of rate-limiting proton transfer (curvatures) at low ArH concentration.

$$A \xrightarrow{k_1} B \xrightarrow{k_2[C]} product$$

$$\frac{d[A]}{dt} = -k_1[A] + k_{-1}[B]$$

$$\frac{d[B]}{dt} = k_1[A] - k_{-1}[B] - k_2[B][C]$$

$$\frac{d[C]}{dt} = -k_2[B][C]$$

 $\begin{array}{l} \text{sol}[k1\_, kn1\_, k2\_, a0\_, c0\_] \coloneqq & \text{NDSolve}[\{a'[t] == -k1*a[t] + kn1*b[t], b'[t] == k1*a[t] - kn1*b[t] - k2*b[t]*c[t], c'[t] == -k2*b[t]*c[t], a[0] == (a0 \ kn1)/(k1 + kn1), b[0] == (a0 \ k1)/(k1 + kn1), c[0] == c0\}, \{a, b, c\}, \{t, 0, 10000\} \end{bmatrix}$ 

Export["table.xls", { Table[Evaluate[c[t] /. sol[0.00001, 0.1, 1000, 0.1, 0.001]], {t, 0, 5000, 1}], Table[Evaluate[c[t] /. sol[0.00001, 0.1, 1000, 0.1, 0.002]], {t, 0, 5000, 1}], Table[Evaluate[c[t] /. sol[0.00001, 0.1, 1000, 0.1, 0.003]], {t, 0, 5000, 1}]}



Figure S4. (Figure 8 in manuscript) Varying degrees of autocatalysis superimposed on first-order decays: curve A, none; curve B, mild; curve C, medium; curve D, strong.

$$A \xrightarrow{k_1} B$$
$$A \xrightarrow{k_2[B]} B$$

$$\frac{d[A]}{dt} = -k_1[A] - k_2[A][B]$$
$$\frac{d[B]}{dt} = k_1[A] + k_2[A][B]$$

 $\{t, 0, 60, 0.3\}$ ]

 $\begin{array}{ll} \text{sol}[k1\_, k2\_, a0\_] := & \text{NDSolve}[\{a'[t] == -k1*a[t] - k2*a[t]*b[t], & b'[t] == k1*a[t] + \\ & k2*a[t]*b[t], a[0] == a0, b[0] == 0\}, \{a, b\}, \{t, 0, 1000\}] \\ \\ & \text{Export}["table.xls", \{Table[Evaluate[a[t] /. sol[0.1, 0, 0.1]], \{t, 0, 60, 0.3\}], \\ & \text{Table}[Evaluate[a[t] /. sol[0.1, 1, 0.1]], \{t, 0, 60, 0.3\}], \\ & \text{Table}[Evaluate[a[t] /. sol[0.1, 5, 0.1]], \\ \end{array}$ 



**Figure S5**. (Figure 9 in manuscript)Simulation of catalysis showing first-order (curve A) and second-order (curve B) saturation kinetics.

rate = 
$$\frac{ax^n}{1+ax^n}$$

Export["table.xls", {Table[1\*x^1/(1 + 1\*x^1), {x, 0, 10, 0.1}], Table[0.2\*x^2/(1 + 0.2\*x^2), {x, 0, 10, 0.1}]}]



**Figure S6**. (Figure 10 in manuscript) Saturation behavior for LiX catalysts. Curve A is a strong catalyst, curve B is a weak catalyst, and curve C corresponds to catalysis with a different deaggregation step than those of curves A and B.

rate = 
$$\frac{ax^n}{1+ax^n}$$

Export["table.xls", {Table[ $5*x^1/(1 + 5*x^1)$ , {x, 0, 10, 0.1}], Table[ $0.2*x^1/(1 + 0.2*x^1)$ , {x, 0, 10, 0.1}], Table[ $0.5*x^1/(1 + 1*x^1)$ , {x, 0, 10, 0.1}]]



Figure S7. (Figure 11 in manuscript) Plot showing preferential metalation of ArH over ArD corresponding to  $k_{\rm H}/k = 24$ .

$$A \xrightarrow{k_{1}} B \xrightarrow{k_{2}[ArH]} \text{ product}$$

$$\frac{d[A]}{dt} = -k_{1}[A] + k_{-1}[B]$$

$$\frac{d[B]}{dt} = k_{1}[A] - k_{-1}[B] - k_{2}[B][ArH] - k_{3}[B][ArD]$$

$$\frac{d[ArH]}{dt} = -k_{2}[B][ArH]$$

$$\frac{d[ArD]}{dt} = -k_{3}[B][ArD]$$

 $sol[k1_, kn1_, k2_, k3_, a0_, h0_, d0_] := NDSolve[\{a'[t] == -k1*a[t] + kn1*b[t], b'[t] == k1*a[t] - kn1*b[t] - k2*b[t]*h[t] - k3*b[t]*d[t], h'[t] == -k2*b[t]*h[t], d'[t] == -k3*b[t]*d[t], a[0] == (a0 kn1)/(k1 + kn1), b[0] == (a0 k1)/(k1 + kn1), h[0] == h0, d[0] == d0\}, {a, b, h, d}, {t, 0, 10000}]$   $Manipulate[ Plot[Evaluate[{h[t], d[t]} /. sol[k1, kn1, k2, k3, a0, h0, d0]], {t, 0, 1000}], {k1, 0, 0001, "k1"}, 0, 1\}, {kn1, 1, "kn1"}, 0, 1\}, {k2, 24000, "k2"}, 0, 1\}, {k3, 1000, "k3"}, 0, 1\}, {a0, 0.1, "a0"}, 0, 1\}, {h0, 0.001, "h0"}, 0, 1\}, {d0, 0.001, "d0"}, 0, 1\}]$   $Export["table.xls", Flatten[Table[ Evaluate[{h[t], d[t]} /. sol[0.0001, 1, 24000, 1000, 0.1, 0.001]], {t, 0, 2000, 1}], 1]]$ 



**Figure S8**. (Figure 17 in manuscript) Simulated plots of concentration versus time for the reaction of 7 (black trace) with lithium diisopropylamide in tetrahydrofuran at – 78 °C. The functions derive from a mathematical model based on Scheme 6.



**Figure S9**. (Figure 18 in manuscript) Simulations of plots showing concentration versus time for various initial concentrations of carbamate 7. The original manuscript simply displayed independent linear fits.

$$\frac{d[\operatorname{ArH}]}{dt} = -k_{1}[\operatorname{ArH}][A_{2}] - k_{3}[\operatorname{A} \cdot \operatorname{ArLi}^{*}][\operatorname{ArH}]$$

$$\frac{d[\operatorname{ArLi}]}{dt} = -k_{4}[\operatorname{ArLi}][A_{2}] + k_{-4}[\operatorname{A} \cdot \operatorname{ArLi}][A_{2}]^{0.5} + 2k_{3}[\operatorname{A} \cdot \operatorname{ArLi}^{*}][\operatorname{ArH}]$$

$$\frac{d[\operatorname{A} \cdot \operatorname{ArLi}]}{dt} = k_{1}[\operatorname{ArH}][A_{2}] - k_{2}[\operatorname{A} \cdot \operatorname{ArLi}] + k_{-2}[\operatorname{A} \cdot \operatorname{ArLi}^{*}] + k_{4}[\operatorname{ArLi}][A_{2}] - k_{-4}[\operatorname{A} \cdot \operatorname{ArLi}][A_{2}]^{0.5}$$

$$\frac{d[\operatorname{A} \cdot \operatorname{ArLi}^{*}]}{dt} = k_{2}[\operatorname{A} \cdot \operatorname{ArLi}] - k_{-2}[\operatorname{A} \cdot \operatorname{ArLi}^{*}] - k_{3}[\operatorname{A} \cdot \operatorname{ArLi}^{*}][\operatorname{ArH}]$$

$$[A_{2}] = \frac{[\operatorname{A}]_{0} - [\operatorname{ArLi}]}{2} - [\operatorname{A} \cdot \operatorname{ArLi}] - [\operatorname{A} \cdot \operatorname{ArLi}^{*}]$$

 $\begin{aligned} & sys[k1_, k2_, kn2_, k3_, k4_, kn4_, a0_, s0_] &:= NDSolve[\{arh'[t] == -k1*arh[t]*a2[t] - k3*aarlis[t]*arh[t], arli'[t] == -k4*arli[t]*a2[t] + kn4*aarli[t]*a2[t]^{0.5 + 2} \\ & k3*aarlis[t]*arh[t], aarli'[t] == k1*arh[t]*a2[t] - k2*aarli[t] + kn2*aarlis[t] + k4*arli[t]*a2[t] - kn4*aarli[t]*a2[t]^{0.5}, aarlis'[t] == k2*aarli[t] - kn2*aarlis[t] + k3*aarlis[t]*arh[t], a2[t] == a0/2 - 0.5*arli[t] - aarlis[t] - aarlis[t], arh[0] == s0, arli[0] == aarlis[0] == 0\}, \{arh, arli, aarli, aarlis, a2\}, \{t, 0, 2000\}] \end{aligned}$ 

Export["carbamate.xls", «insert table from above»]

Manipulate[{Flatten[ Table[Evaluate] arh[t] /. sys[k1, k2, kn2, k3, k4, kn4, a0, 0.001]], {t, 0, 200, 0.5}]], Flatten[ Table[Evaluate] arh[t] /. sys[k1, k2, kn2, k3, k4, kn4, a0, 0.5}]], Flatten[ Table[Evaluate] 0.004]], {t, 0, 200, arh[t] /. sys[k1, k2, kn2, k3, k4, kn4, a0, 0.01]], {t, 0, 200, 0.5}]], Flatten[ Table[Evaluate] arh[t] /. sys[k1, k2, kn2,k3, k4, kn4, a0, 0.02]], {t, 0, 200, 0.5}]], Flatten[ Table[Evaluate] arh[t] / sys[k1]k2, kn2, k3, k4, kn4, a0, 0.03]], {t, 0, 200, 0.5}]], Flatten[ Table[Evaluate] arh[t]/.sys[k1, k2, kn2, k3, k4, kn4, a0, 0.04]], {t, 0, 200, 0.5}]], Flatten[ Table[Evaluate] arh[t] /. sys[k1, k2, kn2, k3, k4, kn4, a0, 0.05]], {t, 0, 200, 0.5]]}, {{k1, 0.020495, "k1"}, 0, 1}, {{k2, 0.09695, "k2"}, 0, 1}, {{kn2, 1.4131, "kn2"}, 0, 1}, {{k3, 828.12, "k3", 0, 1}, {{k4, 0.0461, "k4"}, 0, 1}, {{kn4, 0.0027294, "k1"}, 0, 1}, {{a0, 0.5, "a0"}, 0, 1, {{s0, 0.0074, "s0"}, 0, 1}]

Export["carbamate.xls", «insert table from above»]



Figure S10. (Figure 19 in manuscript) Simulated time-dependent concentrations of ester 11, lithium diisopropylamide dimer 1, enolate homodimer 14, and mixed dimer 16. The functions are from the model described in Scheme 7.

$$\frac{d[ester]}{dt} = -k_2[A][ester]$$

$$\frac{d[A_2]}{dt} = -k_1[A_2] + k_{-1}[A]^2 - k_3[A_2][E] + k_{-3}[A_2][AE]$$

$$\frac{d[A]}{dt} = 2k_1[A_2] - 2k_{-1}[A]^2 - k_2[A][ester] + k_3[A_2][E] - k_{-3}[A][AE] - k_4[A][E] + k_{-4}[AE]$$

$$\frac{d[AE]}{dt} = k_3[A_2][E] - k_{-3}[A][AE] + k_4[A][E] - k_{-4}[AE]$$

$$\frac{d[E]}{dt} = k_2[A][ester] - k_3[A_2][E] + k_{-3}[A][AE] - k_4[A][E] + k_{-4}[AE] - 2k_5[E]^2 + 2k_{-5}[E_2]$$

$$\frac{d[E_2]}{dt} = k_5[E]^2 - k_{-5}[E_2]$$

 $sol[k1_, kn1_, k2_, k3_, kn3_, k4_, kn4_, k5_, kn5_, a0_, s0_] := NDSolve[ \{est'[t] == -k2*a[t]*est[t], a2'[t] == -k1*a2[t] + kn1*a[t]^2 - k3*a2[t]*e[t] + kn3*a[t]*ae[t], a'[t] == 2 k1*a2[t] - 2 kn1*a[t]^2 - k2*a[t]*est[t] + k3*a2[t]*e[t] - kn3*a[t]*ae[t] - k4*a[t]*e[t] + kn4*ae[t], ae'[t] == k3*a2[t]*e[t] - kn3*a[t]*ae[t] + k4*a[t]*e[t] - kn4*ae[t], e'[t] == k2*a[t]*est[t] - k3*a2[t]*e[t] + kn3*a[t]*ae[t] - k4*a[t]*e[t] + kn4*ae[t], e'[t] == k2*a[t]*est[t] - k3*a2[t]*e[t] + kn3*a[t]*ae[t] - k4*a[t]*e[t] + kn4*ae[t], e'[t] == k2*a[t]*est[t] - k3*a2[t]*e[t] + kn3*a[t]*ae[t] - k4*a[t]*e[t] + kn4*ae[t] - 2 k5*e[t]^2 + 2 kn5*e2[t], e2'[t] == k5*e[t]^2 - kn5*e2[t], a2[0] == a0/2, est[0] == s0, a[0] == e[0] == e[0] == e2[0] == 0 \}, \{est, a2, a, ae, e, e2\}, \{t, 0, 20000\} ]$ 

Export["ester.xls", «insert table from above»]



**Figure S11**. (Figure 22 in manuscript) Plot of initial rate versus LiCl concentration showing catalyzed inhibition (scenario 1), no change in rate (scenario 2), and catalyzed acceleration (scenario 3).

$$\frac{d[A_{2}]}{dt} = -k_{1}[A_{2}] + k_{-1}[A_{2}^{*}] - (k_{2} + k_{5}[LiX])[A_{2}] + (k_{-2} + \frac{k_{5}k_{-2}}{k_{2}}[LiX])[A]^{2}$$

$$\frac{d[A_{2}^{*}]}{dt} = k_{1}[A_{2}] - k_{-1}[A_{2}^{*}] - k_{3}[A_{2}^{*}][S]$$

$$\frac{d[A]}{dt} = 2(k_{2} + k_{5}[LiX])[A_{2}] - 2(k_{-2} + \frac{k_{5}k_{-2}}{k_{2}}[LiX])[A]^{2} - k_{4}[A][S] + k_{3}[A_{2}^{*}][S]$$

$$\frac{d[S]}{dt} = -k_{3}[A_{2}^{*}][S] - k_{4}[A][S]$$

 $sol[k1, kn1, k2, kn2, k3, k4, k5, a0, s0, c] := NDSolve[{a2'[$ t] == -(k1) a2[t]  $t + (kn2 + k5*kn2/k2*c) a[t]^2, a2s'[t] == (k1) a2[t] - (k1) a2[t] + (kn1) a_{2s}[t] - (k_{2} + k_{5}*c) a_{2}[t]$ (kn1) a2s[t] - k3\*a2s[t]\*s[t],a'[t] ==  $2 (k2 + k5*c) a2[t] - 2 (kn2 + k5*kn2/k2*c) a[t]^2$ s'[t] = -k3\*a2s[t]\*s[t] - k4\*a[t]\*s[t],k4\*a[t]\*s[t] + k3\*a2s[t]\*s[t],a2[0] == (4) $a0 \text{ kn1} + (k2 \text{ kn1}^2)/(k1 \text{ kn2} + \text{ kn1} \text{ kn2}) - ($ Sqrt[k2] kn1 $^(3/2)$  Sqrt[k2 kn1 + 8 a0 k1 kn2 + 8 a0 kn1 kn2)/( k1 kn2 + kn1 kn2))/(8 (k1 + kn1)), a2s[0] == ( 4 a0 k1 + (k1 k2))/(8 (k1 + kn1))) kn1)/(k1 kn2 + kn1 kn2) - (k1 Sqrt[k2] Sqrt[kn1] Sqrt[ k2 kn1 + 8 a0 k1 kn2 + 8 a0 kn1 kn2)/(k1 kn2 + kn1 kn2)/( 8 (k1 + kn1)), a[0] == (-k2 kn1 + kn1)Sqrt[k2] Sqrt[kn1] Sqrt[k2 kn1 + 8 a0 k1 kn2 + 8 a0 kn1 kn2])/(4 (k1 kn2 + kn1 kn2)), s[0] == s0, {a2, a2s, a, s}, {t, 0, 10000}]

# III. Parallel versus Serial Barrier Order Dependence



Figure S12. Order in LDA versus  $\Delta G$  (parallel)



$$\frac{d[A_{2}]}{dt} = -k_{1}[A_{2}] + k_{-1}[A_{2}^{*}] - 2k_{1}k_{2}[A_{2}]^{2} + 2\frac{k_{1}k_{2}}{K}[A_{4}] + \frac{k_{3}}{2}[A_{2}^{*}][S] + \frac{3k_{4}}{2}[A_{4}][S]$$

$$\frac{d[A_{2}^{*}]}{dt} = k_{1}[A_{2}] - k_{-1}[A_{2}^{*}] - k_{3}[A_{2}^{*}][S]$$

$$\frac{d[A_{4}]}{dt} = k_{1}k_{2}[A_{2}]^{2} - \frac{k_{1}k_{2}}{K}[A_{4}] - k_{4}[A_{4}][S]$$

$$\frac{d[S]}{dt} = -k_{3}[A_{2}^{*}][S] - k_{4}[A_{4}][S]$$

Solve[ $\{-k1*a2 + kn1*a2s == 0, -2 k2*k1*a2^2 + 2*k2*k1*a4/Keq == 0, 2 a2 + 2 a2s + 4 a4 == a0\}, \{a2, a2s, a4\}$ ]

 $sol2[k1_, kn1_, k2_, Keq_, k3_, k4_, a0_, s0_] := NDSolve[{a2'[t] == -k1*a2[t] + kn1*a2s[t] - 2 k2*k1*a2[t]^2 + 2*k2*k1*a4[t]/Keq + 1/2 k3*a2s[t]*s[t] + 3/2*k4*a4[t]*s[t], a2s'[t] == k1*a2[t] - kn1*a2s[t] - k3*a2s[t]*s[t], a4'[t] == k2*k1*a2[t]^2 - k2*k1*a4[t]/Keq - k4*a4[t]*s[t], s'[t] == -k3*a2s[t]*s[t] - k4*a4[t]*s[t], a2[0] == (-k1 - kn1 + Sqrt[ k1^2 + 2 k1 kn1 + kn1^2 + 4 a0 Keq kn1^2])/(4 Keq kn1), a2s[0] == (-(k1/Keq) - k1^2/(Keq kn1) + (k1 Sqrt[k1^2 + 2 k1 kn1 + kn1^2 + 4 a0 Keq kn1^2])/(4 Keq kn1), a4[0] == ((2 k1)/Keq + k1^2/(Keq kn1) + 2 a0 kn1 + kn1/ Keq - Sqrt[k1^2 + 2 k1 kn1 + kn1^2 + 4 a0 Keq kn1^2]/(Keq kn1) + (k1 Sqrt[k1^2 + 2 k1 kn1 + kn1/ kn1^2 + 2 k1 kn1 + kn1/ kn1^2 + 4 a0 Keq kn1^2])/(Keq kn1))/((keq kn1))/((keq kn1))/((keq kn1))/((keq kn1))/((keq kn1))/((keq kn1)))/((keq kn1))/((keq kn1))/((keq kn1))/((keq kn1)))/((keq kn1))/((keq kn1)))/((keq kn1))/((keq kn1))/((keq kn1)))/((keq kn1))/((keq kn1))/((keq kn1)))/((keq kn1))/((keq kn1))/((keq kn1)))/((keq kn1))/((keq kn1)))/((keq kn1))/((keq kn1)))/((keq kn1))/((keq kn1))/((keq kn1))/((keq kn1)))/((keq kn1))/((keq kn1))/((keq kn1))/((keq kn1))/((keq kn1))/((keq kn1))/((keq kn1)))/((keq kn1))/((keq kn1))/((k$ 

 $\begin{array}{ll} Manipulate[\{Plot[-s'[1] /. sol2[k1, kn1, Exp[-4186.8 g/(8.314*195.13)], keq1, k3, k4, a0, s0], \{a0, 0, 10\}], & Plot[Evaluate[\{s[t]\} /. sol2[k1, kn1, Exp[-4186.8 g/(8.314*195.13)], keq1, k3, k4, a0, s0]], \{t, 0, 1000\}, PlotRange -> \{0, 0.01\}]\}, \{\{k1, 0.00001, "k1"\}, 0, 10\}, \{\{kn1, 10, "kn1"\}, 0, 1000\}, \{\{g, 0, "g"\}, -10, 10\}, \{\{keq1, 1.`*^-12, "Keq1"\}, 0, 1000\}, \{\{k3, 10000, "k3"\}, 0, 1000\}, \{\{k4, 100000000, "k4"\}, 0, 1000\}, \{\{a0, 0.1, "a0"\}, 0, 1\}, \{\{s0, 0.01, "s0"\}, 0, 1\}] \end{array}$ 

 $\begin{array}{ll} Flatten[Table[{g, a}] /. & FindFit[Flatten[ Table[{10^a0, Log[-s'[0.1]]}] /. \\ sol2[0.000001, 1, Exp[-4186.8 g/(8.314*195.13)], 1.`*^-12, & 10000, 1000000000, \\ 10^(a0), 0.01], {a0, -1, 1, 0.01}]], & a*Log[x] + b, {a, b}, x], {g, -3, 3, 1}], 0] \end{array}$ 



Figure S13. Order in LDA versus  $\Delta G$  (series)



$$\frac{d[A_{2}]}{dt} = -k_{1}[A_{2}] + k_{-1}[A_{2}^{*}] - k_{-1}k_{2}[A_{2}][A_{2}^{*}] + \frac{k_{-1}k_{2}}{K}[A_{4}] + \frac{3k_{3}}{2}[A_{4}][S]$$

$$\frac{d[A_{2}^{*}]}{dt} = k_{1}[A_{2}] - k_{-1}[A_{2}^{*}] - k_{-1}k_{2}[A_{2}][A_{2}^{*}] + \frac{k_{-1}k_{2}}{K}[A_{4}]$$

$$\frac{d[A_{4}]}{dt} = k_{-1}k_{2}[A_{2}][A_{2}^{*}] - \frac{k_{-1}k_{2}}{K}[A_{4}] - k_{3}[A_{4}][S]$$

$$\frac{d[S]}{dt} = -k_{3}[A_{4}][S]$$

Solve[ $\{k1*a2 - kn1*a2s == 0, -k2*kn1*a2*a2s + k2*kn1/Keq1*a4 == 0, 2a2 + 2a2s + 4a4 == a0\}, \{a2, a2s, a4\}$ ]

 $sol[k1, kn1, k2, Keq1, k3, a0, s0] := NDSolve[{a2'[t] == -k1*a2[t] + kn1*a2s[t] - kn1*a2s[t]$ k1\*a2[t] k2\*kn1\*a2[t]\*a2s[t] +k2\*kn1/Keq1\*a4[t] + 3/2\*k3\*a4[t]\*s[t], a2s'[t] ==kn1\*a2s[t] - k2\*kn1\*a2[t]\*a2s[t] + k2\*kn1/Keq1\*a4[t], a4'[t] == k2\*kn1\*a2[t]\*a2s[t] - k2\*kn1\*a2[t]\*a2s[t]\*a2s[t] - k2\*kn1\*a2[t]\*a2s[t] - k2\*kn1\*a2[t]\*a2 $k^{2}kn^{1}/Keq^{1}a^{4}[t] - k^{3}a^{4}[t]s^{t}], s'[t] = -k^{3}a^{4}[t]s^{t}], a^{2}[0] = (-k^{1} - kn^{1} + Sqrt[t]s^{t}], a^{2}[0] = (-k^{1} - kn^{1}$  $k1^{2} + 2 k1 kn1 + 4 a0 k1 Keq1 kn1 + kn1^{2})/(4 k1 Keq1), a2s[0] == (-(k1/Keq1) - (k1/Keq1))/(4 k1 Keq1), a3s[0] = (-(k1/Keq1) - (k1/Keq1))/(4 k1 Keq1), a3s[0] = (-(k1/Keq1) - (k1/Keq1))/(4 k1 Keq1), a3s[0] = (-(k1/Keq1) - (k1/Keq1))/(4 k1 Keq1))/(4 k1 Keq1)$ a4[0] kn1/Keq1 + Sqrt[  $k1^2 + 2 k1 kn1 + 4 a0 k1 Keq1 kn1 + kn1^2]/Keq1)/(4 kn1),$ ==  $1/(8 \text{ kn1}) (k1/\text{Keg1} + 2 a0 \text{ kn1} + (2 \text{ kn1})/\text{Keg1} + \text{kn1}^2/(k1 \text{ Keg1}) Sart[k1^2 + 2]$  $k1 kn1 + 4 a0 k1 Keq1 kn1 + kn1^2]/Keq1 - ($ kn1 Sqrt[ $k1^{2} + 2 k1 kn1 + 4 a0 k1$  Keq1  $kn1 + kn1^2)/($ k1 Keq1), s[0] == s0,  $\{a2, a2s, a4, s\}$ ,  $\{t, 0, 10000\}$ 

 $\begin{array}{ll} Manipulate[\{Plot[-s'[1] /. sol[k1, kn1, Exp[-4186.8 g/(8.314*195.13)], keq1, k3, a0, s0], \{a0, 0, 10\}], & Plot[Evaluate[\{s[t]\} /. sol[k1, kn1, Exp[-4186.8 g/(8.314*195.13)], keq1, k3, a0, s0]], \{t, 0, 1000\}, PlotRange -> \{0, 0.01\}], & Flatten[Table[\{g, a\} /. FindFit[Flatten[ Table[Log[-s'[1]] /. sol[k1, kn1, Exp[-4186.8 g/(8.314*195.13)]], keq1, k3, a0, s0], <math>\{a0, 0.01, 10, 0.01\}$ ]], a\*Log[x] + b,  $\{a, b\}$ , x],  $\{g, -3, 3, 1\}$ ], 0]},  $\{\{k1, 0.001, "k1"\}, 0, 100\}, \{\{kn1, 1000, "kn1"\}, 0, 1000\}, \{\{keq1, 1, "Keq1"\}, 0, 1000\}, \{\{k3, 100000000, "k3"\}, 0, 1000\}, \{\{a0, 0.1, "a0"\}, 0, 1\}, \{\{g, 0, "g"\}, -3, 3\}, \{\{s0, 0.01, "s0"\}, 0, 1\} \end{bmatrix}$ 

Flatten[Table[{g, a} /. FindFit[Flatten[ 4186.8 g/(8.314\*195.13)], 1, 100000000, b, {a, b}, x], {g, -3, 3, 0.1}], 0] Table[Log[-s'[1]] /. sol[0.001, 1000, Exp[a0, 0.01], {a0, 0.01, 10, 0.01}]], a\*Log[x] +

# IV. Standard Steady State Treatment of Multiple Barriers in Series



Assume the forward rate constant for conversion of A to  $Y_0$  is  $k_1$  and the reverse rate constant is  $k_{-1}$ . All intermediates  $Y_i$  are of the same energy; otherwise stated, they are pairwise interconverted with rate constant  $k_{-1}$ . The time-varying concentration of  $Y_i$  is:

$$\frac{d[\mathbf{Y}_i]}{dt} = k_{-1}[\mathbf{Y}_{i-1}] - 2k_{-1}[\mathbf{Y}_i] + k_{-1}[\mathbf{Y}_{i+1}]$$
Assuming a steady state has been reached  $\frac{d[\mathbf{Y}_i]}{dt} = 0$ , and

$$[\mathbf{Y}_{i-1}] = 2[\mathbf{Y}_i] - [\mathbf{Y}_{i+1}] \tag{1a}$$

On shifting the index,

$$[\mathbf{Y}_{i}] = 2[\mathbf{Y}_{i+1}] - [\mathbf{Y}_{i+2}]$$
(1b)

From equation 1b, it follows that  $[Y_{m-1}] = 2[Y_m]$  and generally that

$$[Y_{m-x}] = (x+1)[Y_m]$$
(2)

The time-varying concentration of Y<sub>0</sub> is

$$\frac{d[\mathbf{Y}_0]}{dt} = k_1[\mathbf{A}] - 2k_{-1}[\mathbf{Y}_0] + k_{-1}[\mathbf{Y}_1]$$

Applying the steady state approximation to the former expression gives

$$[\mathbf{Y}_{0}] = \frac{k_{1}[\mathbf{A}] + k_{-1}[\mathbf{Y}_{1}]}{2k_{-1}}$$
(3)

Using equation 1b for  $[Y_0]$  we find  $[Y_0] = 2[Y_1] - [Y_2]$ . Given that  $\frac{[Y_2]}{[Y_1]} = \frac{m-1}{m}$  from equation 2,  $[Y_0] = 2[Y_1] - \frac{m-1}{m}[Y_1] = \left(2 - \frac{m-1}{m}\right)[Y_1]$ . Therefore,

$$[Y_1] = \frac{[Y_0]}{\left(2 - \frac{m-1}{m}\right)}$$
(4)

On combining equations 3 and 4,

$$[Y_0] = \frac{k_1[A] + k_{-1} \left( \frac{[Y_0]}{\left(2 - \frac{m-1}{m}\right)} \right)}{2k_{-1}}$$

Simplification of the above gives

$$[Y_0] = \frac{k_1[A]}{k_{-1}} \left( \frac{1}{2 - \frac{1}{2 - \frac{m-1}{m}}} \right)$$
$$= \frac{k_1[A]}{k_{-1}} \left( \frac{m+1}{m+2} \right)$$

To obtain an expression for the rate of consumption of [A] as a function of relevant rate constants and the number of barriers begin with the rate law for A and employ the preceding result:

$$\frac{d[A]}{dt} = -k_1[A] + k_{-1}[Y_0]$$
  
=  $-k_1[A] + k_{-1}\left(\frac{k_1[A]}{k_{-1}}\left(\frac{m+1}{m+2}\right)\right)$   
=  $-k_1\left(1 - \frac{m+1}{m+2}\right)[A]$   
=  $-k_1\left(\frac{1}{m+2}\right)[A]$ 

Notice that the number of barriers is m+2, so we define n = m+2, and the above expression becomes

$$\frac{\mathrm{d}[\mathrm{A}]}{\mathrm{d}t} = -\frac{k_1}{n}[\mathrm{A}] \tag{5}$$

Therefore, the rate of a process that proceeds through n barriers of equal activation energy relative to the ground state attenuates the rate associated with reactivity through a single such barrier by a factor of n.

Proof of equation 2:

We want to show that  $[Y_{m-x}] = (x+1)[Y_m]$ , so we provisionally assume that  $[Y_{m-x}] = (x+1)[Y_m]$  and  $[Y_{m-(x-1)}] = x[Y_m]$  are true. From equation 1a, we know that  $[Y_{i-1}] = 2[Y_i] - [Y_{i+1}]$ , so  $[Y_{m-(x+1)}] = 2[Y_{m-x}] - [Y_{m-(x-1)}] = 2(x+1)[Y_m] - x[Y_m] = (x+2)[Y_m]$  and the proof is complete.

# V. Arbitrary Height Barriers in Series

We want to derive a general expression for overall rate in terms of the microscopic rate constants and do so paralleling Wagner, C. *Advances in Catalysis*, **1970**, *21*, 323. Consider the scheme depicted below.

$$C \xrightarrow{k_1} I_1 \xrightarrow{k_2} \dots \xrightarrow{k_n} P$$

At each step, denote  $K_i = k_i/k_{-i}$ . Assume that a single rate-limiting step exists at position *m*, for which all preceding and subsequent steps are at equilibrium. By mass balance,

$$\begin{bmatrix} \mathbf{I}_{m-1} \end{bmatrix}^* = \begin{bmatrix} \mathbf{C} \end{bmatrix} \prod_{i=1}^{m-1} K_i$$
$$\begin{bmatrix} \mathbf{I}_m \end{bmatrix}^* = \begin{bmatrix} \mathbf{P} \end{bmatrix} \prod_{i=m+1}^n K_i^{-1}$$

Given that  $K_{eq} = \prod_{i=1}^{n} K_i$ , a rate expression assuming exclusive rate-limitation at position *m* follows.

$$v_m^* = k_m \left( \left[ \mathbf{I}_{m-1} \right]^* - \frac{\left[ \mathbf{I}_{m-1} \right]^*}{K_m} \right)$$
$$= k_m \left( \left[ \mathbf{C} \right] \prod_{i=1}^{m-1} K_i - \frac{\left[ \mathbf{P} \right] \prod_{i=m+1}^n K_i^{-1}}{K_m} \right)$$
$$= k_m \prod_{i=1}^{m-1} K_i \left( \left[ \mathbf{C} \right] - \left[ \mathbf{P} \right] \prod_{i=1}^n K_i^{-1} \right)$$
$$= k_m \prod_{i=1}^{m-1} K_i \left( \left[ \mathbf{C} \right] - \frac{\left[ \mathbf{P} \right]}{K_{eq}} \right)$$

The overall rate at steady state is given by

$$v = v_m = k_m \left( \begin{bmatrix} \mathbf{I}_{m-1} \end{bmatrix} - \frac{\begin{bmatrix} \mathbf{I}_{m-1} \end{bmatrix}}{K_m} \right)$$

We are now in a position to relate v to the various  $v^*$ . Begin by finding the ratio  $\frac{v_m}{v_m^*}$ .

$$\frac{v_m}{v_m^*} = \frac{k_m \left( \begin{bmatrix} \mathbf{I}_{m-1} \end{bmatrix} - \frac{\begin{bmatrix} \mathbf{I}_m \end{bmatrix}}{K_m} \right)}{k_m \prod_{i=1}^{m-1} K_i \left( \begin{bmatrix} \mathbf{C} \end{bmatrix} - \frac{\begin{bmatrix} \mathbf{P} \end{bmatrix}}{K_{eq}} \right)}$$
$$= \frac{\prod_{i=1}^{m-1} K_i^{-1} \left( \begin{bmatrix} \mathbf{I}_{m-1} \end{bmatrix} - \frac{\begin{bmatrix} \mathbf{I}_m \end{bmatrix}}{K_m} \right)}{\left( \begin{bmatrix} \mathbf{C} \end{bmatrix} - \frac{\begin{bmatrix} \mathbf{P} \end{bmatrix}}{K_{eq}} \right)}$$

Sum over all 
$$\frac{v_m}{v_m^*}$$
.  

$$\sum_{m=1}^{n} \frac{v_m}{v_m^*} = \sum_{m=1}^{n} \frac{\prod_{i=1}^{m-1} K_i^{-1} \left( [\mathbf{I}_{m-1}] - \frac{[\mathbf{I}_m]}{K_m} \right)}{[\mathbf{C}] - \frac{[\mathbf{P}]}{K_{eq}}}$$

$$= \frac{1}{[\mathbf{C}] - \frac{[\mathbf{P}]}{K_{eq}}} \left( \sum_{m=1}^{n} \prod_{i=1}^{m-1} K_i^{-1} [\mathbf{I}_{m-1}] - \sum_{m=1}^{n} \prod_{i=1}^{m} K_i^{-1} [\mathbf{I}_m] \right)$$
note that  $[\mathbf{I}_0]$  is  $[\mathbf{C}]$  and  $[\mathbf{I}_n]$  is  $[\mathbf{P}]$ 

$$= \frac{1}{[\mathbf{C}] - \frac{[\mathbf{P}]}{K_{eq}}} \left( [\mathbf{C}] + \sum_{m=2}^{n} \prod_{i=1}^{m-1} K_i^{-1} [\mathbf{I}_{m-1}] - \sum_{m=1}^{n-1} \prod_{i=1}^{m} K_i^{-1} [\mathbf{I}_m] - \frac{[\mathbf{P}]}{K_{eq}} \right)$$

$$= \frac{1}{[\mathbf{C}] - \frac{[\mathbf{P}]}{K_{eq}}} \left( [\mathbf{C}] + \sum_{m=1}^{n-1} \prod_{i=1}^{m} K_i^{-1} [\mathbf{I}_m] - \sum_{m=1}^{m-1} \prod_{i=1}^{m} K_i^{-1} [\mathbf{I}_m] - \frac{[\mathbf{P}]}{K_{eq}} \right)$$

$$= \frac{[\mathbf{C}] - \frac{[\mathbf{P}]}{K_{eq}}}{[\mathbf{C}] - \frac{[\mathbf{P}]}{K_{eq}}}$$

$$= 1$$

With this trivial identity, proceed to find the overall reaction rate.

$$\sum_{m=1}^{n} \frac{v_m}{v_m^*} = \sum_{m=1}^{n} \frac{v}{v_m^*} = v \sum_{m=1}^{n} \frac{1}{v_m^*} = 1$$
  
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Therefore,



Under initial rate conditions, assume  $[P] \approx 0$  to give the expression below (equation 32 in the manuscript)



# Particular Cases.

### 1) Equivalent–Energy Intermediates

We examine the case where all intermediates in the conversion of C to P are of equal energy. This means  $1 = K_2 = K_3 = ... = K_{n-1}$ . Therefore,

$$-\frac{d[C]}{dt} = \frac{[C]_{0}}{\frac{1}{k_{1}} + \sum_{m=2}^{n} \frac{1}{k_{m}K_{1}}}$$
$$= \frac{k_{1}[C]_{0}}{1 + \frac{k_{1}}{K_{1}} \sum_{m=2}^{n} \frac{1}{k_{m}}}$$
$$= \frac{k_{1}[C]_{0}}{1 + k_{-1} \sum_{m=2}^{n} \frac{1}{k_{m}}}$$

2) Equivalent–Energy Intermediates and Barriers of Equal Height

$$-\frac{d[C]}{dt} = \frac{k_1[C]_0}{1+k_{-1}\sum_{m=2}^n \frac{1}{k_{-1}}}$$
$$= \frac{k_1[C]_0}{1+\sum_{m=2}^n 1}$$
$$= \frac{k_1[C]_0}{n}$$

3) Differing Molecularity — Two Barrier Case

A 
$$\underset{k_{-1}}{\underbrace{k_1}}$$
 I  $\underset{k_{-2}}{\underbrace{k_2[S]}}$  product

Following the equation described in the previous section,

$$\frac{d[product]}{dt} = \frac{[A]_{0}}{\sum_{m=1}^{n} \frac{1}{k_{m} \prod_{i=1}^{m-1} K_{i}}}$$
$$= \frac{[A]_{0}}{\frac{1}{k_{1}} + \frac{1}{k_{2}[S]\left(\frac{k_{1}}{k_{-1}}\right)}}$$
$$= \frac{k_{1}k_{2}[A]_{0}[S]}{k_{-1} + k_{2}[S]}$$

As expected from a standard steady state treatment.

# **VI. Complete Reference 18**

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